

## Step 1. Determining conditions required for the design

- Machine type
- Transmission power, or rated power of the driving machine
- Degree of load fluctuation
- Daily operating hours
- Speed ratio

$$\left( \frac{\text{Pinion revolution}}{\text{Revolution of large pulley}} \right)$$

- Temporary center distance
- Pulley diameter restriction
- Operating environment (high temperature, low temperature, oil, water, dirt, acid, alkali)

## Step 2. Calculating the design power

Calculate the design power with [Formula 1](#).

**Formula 1**

$$Pd = Pt \times (Ko + Ki + Ke)$$

Pd : Design power (kW)  
 Pt : Transmission power<sup>Note 1</sup> (kW)  
 Ko : Load correction factor (Table 1 → P. 247)  
 Ki : Idler correction factor (Table 2 → P. 247)  
 Ke : Environment correction factor (Table 3 → P. 247)

**Note 1)** For transmission power, it is ideal to use the load of the driven machine; however, if it is unknown, use the rated power of the driving machine. If torque or horsepower is used for indication, convert it into watt or kilowatt using [Formula 2](#).

**Formula 2**

$$Pt = \frac{Tr \times n}{9550}$$

Pt : Transmission power (kW)  
 n : Revolution (rpm)  
 Tr : Load torque (N·m)  
 1PS=0.7355(kW)

## Step 3. Selecting a belt type

Obtain a belt type based on the design power and pinion revolution from [Fig. 1 "Belt type selection diagram"](#) (→ P. 247 to P. 248).

If an obtained type is close to the line of intersection of two types, design both belt types as a trial and choose the one that matches the purpose of the design and that is the more economical.

## Step 4. Selecting a pulley diameter

Select an appropriate pulley diameter with [Formula 3](#), taking the restriction of the power transmission space etc. into consideration.

■ In the cases of V-belts, Power Ace, and Power Ace Cog

**Formula 3**

$$Dp = \frac{n_1}{n_2} \times dp$$

$$\text{Speed ratio} = \frac{n_1}{n_2}$$

dp : Pinion pitch diameter (mm)  
 Dp : Large pulley pitch diameter (mm)  
 n<sub>1</sub> : Pinion revolution (rpm)  
 n<sub>2</sub> : Large pulley revolution (rpm)

The relationship between pulley nominal outside diameter and pulley pitch diameter is based on [Table 4](#) (→ P. 249).

■ In the case of Rib-Ace

**Formula 3**

$$Do = \frac{n_1}{n_2} \times do$$

$$\text{Speed ratio} = \frac{n_1}{n_2}$$

do : Pinion outside diameter (mm)  
 Do : Large-pulley outside diameter (mm)  
 n<sub>1</sub> : Pinion revolution (rpm)  
 n<sub>2</sub> : Large pulley revolution (rpm)

When you determine a pulley diameter, check the following items:

- Check of the belt speed

Calculate the belt speed with [Formula 4](#).

■ In the cases of V-belts, Power Ace, and Power Ace Cog

**Formula 4**

$$v = \frac{dp \times n}{19100}$$

v : Belt speed (m/s)  
 dp : Pinion pitch diameter (mm)  
 n : Pinion revolution (rpm)

■ In the case of Rib-Ace

**Formula 4**

$$v = \frac{do \times n}{19100}$$

v : Belt speed (m/s)  
 do : Pinion outside diameter (mm)  
 n : Pinion revolution (rpm)

The belt speed needs to satisfy [Table 6](#) (→ P. 249).

If the belt speed exceeds the standard, reduce the pulley diameter.

**Note 2)**

If the belt speed exceeds the value in the following table, you need to take a dynamic balance of the pulley. In this case, use rolled steel for general structure or carbon steel for machine construction.

	Power Ace	Rib-Ace 2
Belt speed	30m/s	35m/s

- Check of the minimum nominal outside diameter of a pulley

Generally, when a pulley with a small diameter is used, the flex fatigue of the belt increases, reducing the belt service life.

Therefore, it is ideal to at least use a pulley diameter equal to or larger than the minimum nominal outside diameter of a pulley indicated in [Table 5 "Minimum pulley diameters"](#) (→ P. 249).

## Step 5. Selecting an effective length

Calculate a rough effective length L' with [Formula 5](#) and select an effective length that is closest to this value from the standard size of the respective belt.

■ In the case of V-belts (Table of standard sizes → P. 232 to P. 233)

**Formula 5**

$$L' = 2C' + 1.57(Dp + dp) + \frac{(Dp - dp)^2}{4C'}$$

L' : Rough effective length (mm)  
 C' : Temporary center distance (mm)  
 Dp : Large pulley pitch diameter (mm)  
 dp : Pinion pitch diameter (mm)

■ In the cases of Power Ace / Power Ace Cog / Power Ace Aramid Combo / Rib-Ace (Table of standard sizes → P. 230, P. 236)

**Formula 5**

$$L' = 2C' + 1.57(Do + do) + \frac{(Do - do)^2}{4C'}$$

L' : Rough effective length (mm)  
 C' : Temporary center distance (mm)  
 Do : Large-pulley nominal outside diameter (Power Ace / Power Ace Cog / Power Ace Aramid Combo) (mm)  
 Large-pulley outside diameter (Rib-Ace) (mm)  
 do : Pinion nominal outside diameter (Power Ace / Power Ace Cog / Power Ace Aramid Combo) (mm)  
 Pinion outside diameter (Rib-Ace) (mm)

- Calculation of the center distance

From the selected effective length, backcalculate the center distance with [Formula 6](#).

■ In the case of V-belts

**Formula 6**

$$C = \frac{B + \sqrt{B^2 - 2(Dp - dp)^2}}{4}$$

$$B = Le - 1.57(Dp + dp)$$

C : Center distance (mm)  
 Le : Effective length (mm)  
 Dp : Large pulley pitch diameter (mm)  
 dp : Pinion pitch diameter (mm)

■ In the cases of Power Ace / Power Ace Cog / Power Ace Aramid Combo / Rib-Ace

**Formula 6**

$$C = \frac{B + \sqrt{B^2 - 2(Do - do)^2}}{4}$$

$$B = Le - 1.57(Do + do)$$

C : Center distance (mm)  
 Le : Effective length (mm)  
 Do : Large-pulley nominal outside diameter (Power Ace / Power Ace Cog / Power Ace Aramid Combo) (mm)  
 Large-pulley outside diameter (Rib-Ace) (mm)  
 do : Pinion nominal outside diameter (Power Ace / Power Ace Cog / Power Ace Aramid Combo) (mm)  
 Pinion outside diameter (Rib-Ace) (mm)

**Note 3)** For Power Ace, Power Ace Cog, and Power Ace Aramid Combo, Le = effective outside length.

## Step 6. Calculating the number of belts and the number of ribs

① Determination of the basic power rating

Obtain the basic power rating for the pinion diameter and its revolution from the [tables of basic power ratings](#) (P. 250 to P. 270). Add an "additional transmission capacity by the speed ratio" in the lower table and set it as the basic power rating per belt or per rib.

② Correction of the basic power rating

From [Table 7](#) (→ P. 271), obtain the correction factor KI by the effective length.

From [Formula 7](#), obtain the angle of contact of the pinion θ<sub>1</sub> and from [Table 8](#) (→ P. 272), obtain the correction factor Kθ<sub>1</sub>.

■ In the case of V-belts

**Formula 7**

$$\theta_1 = 180 - \frac{57(Dp - dp)}{C}$$

θ<sub>1</sub> : Angle of contact of pinion (°)  
 Dp : Large pulley pitch diameter (mm)  
 dp : Pinion pitch diameter (mm)  
 C : Center distance (mm)

■ In the cases of Power Ace / Power Ace Cog / Power Ace Aramid Combo / Rib-Ace

**Formula 7**

$$\theta_1 = 180 - \frac{57(Do - do)}{C}$$

θ<sub>1</sub> : Angle of contact of pinion (°)  
 Do : Large-pulley nominal outside diameter (Power Ace / Power Ace Cog / Power Ace Aramid Combo) (mm)  
 Large-pulley outside diameter (Rib-Ace) (mm)  
 do : Pinion nominal outside diameter (Power Ace / Power Ace Cog / Power Ace Aramid Combo) (mm)  
 Pinion outside diameter (Rib-Ace) (mm)  
 C : Center distance (mm)

③ Calculating the number of belts

Calculate the number of belts with [Formula 8](#). Round up the figures after the decimal point to an integer.

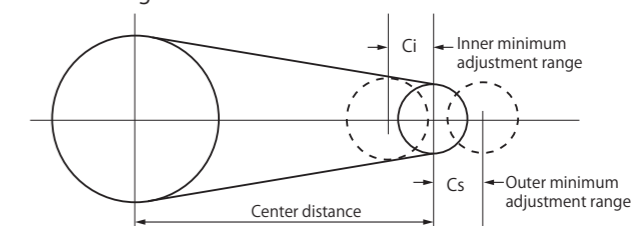
**Formula 8**

$$N = \frac{Pd}{Pr \times KI \times K\theta_1}$$

N : No. of belts (pcs) or (No. of ribs)  
 Pd : Design power (kW)  
 Pr : Basic power rating (kW/pc) or (kW/rib)  
 KI : Length correction factor (Table 7 → P. 271)  
 Kθ<sub>1</sub> : Pinion contact angle correction factor (Table 8 → P. 272)

## Step 7. Checking the adjustment range of the center distance

From [Table 9](#) (→ P. 272), obtain the installation range and the tension range of the belt.



**Table 1 Load correction factor (K<sub>o</sub>)**

Driven machine		Driving machine					
		Starting torque less than 300%			Starting torque 300% or more		
		AC motor (normal torque, squirrel-cage type, synchronous electric) DC motor (shunt-wound)			AC motor (high torque / single-phase / series-wound) DC motor (compound-wound, series-wound) Engine / line shaft / clutch		
		I	II	III	I	II	III
A	<ul style="list-style-type: none"> <li>Fluid stirring machines</li> <li>Centrifugal pumps</li> <li>Fans of 7.5 kW or less</li> <li>Blowers</li> <li>Compact compressors</li> <li>Light-duty conveyors</li> <li>Exhausters</li> </ul>	1.0	1.1	1.2	1.1	1.2	1.3
	<ul style="list-style-type: none"> <li>Sand and grain conveyors</li> <li>Fans of 7.5 kW or more</li> <li>Line shafts</li> <li>Punches, presses, shearers</li> <li>Rotary/vibrating sieves</li> <li>Kneading mixers</li> <li>Generators</li> <li>Laundry machines</li> <li>Printing machines</li> <li>Rotary pumps</li> <li>Machine tools</li> </ul>	1.1	1.2	1.3	1.2	1.3	1.4
C	<ul style="list-style-type: none"> <li>Brick-processing machines</li> <li>Exciters</li> <li>Hammer mills</li> <li>Piston pumps</li> <li>Pulverizers</li> <li>Saw mills, Woodworking machines</li> <li>Fabric machines</li> <li>Bucket elevators</li> <li>Conveyors</li> <li>Papermaking mills, heaters</li> <li>Forced portable blowers</li> <li>Saw mills, Woodworking machines</li> </ul>	1.2	1.3	1.4	1.4	1.5	1.6
	<ul style="list-style-type: none"> <li>Sand pumps</li> <li>Mills (ball, rod, tube)</li> <li>Hoists</li> <li>Crashers</li> <li>Rubber calenders, Extruders</li> </ul>	1.3	1.4	1.5	1.5	1.6	1.8

Note)  
I: Intermittent use (3 to 5 hrs/day or seasonal use)  
II: Normal use (8 to 10 hrs/day)  
III: Continuous use (16 to 24 hrs/day)

**Table 2 Idler correction factor (K<sub>i</sub>)**

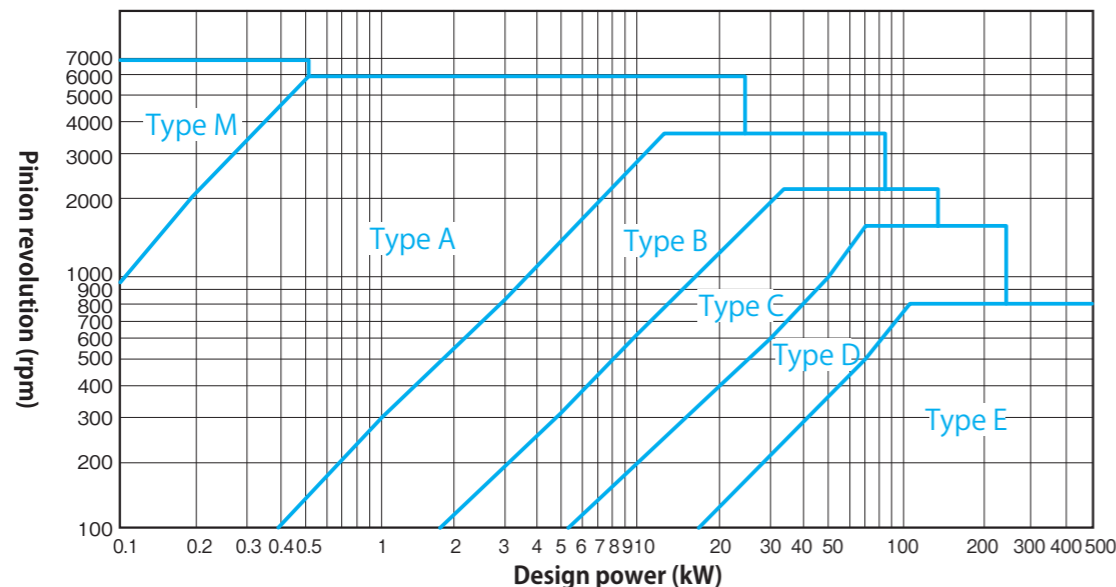
Idler installation location	K <sub>i</sub>
- No idlers	0.0
- Installed from the inside on the slack side	0.0
- Installed from the outside on the slack side	0.1
- Installed from the inside on the tight side	0.1
- Installed from the outside on the tight side	0.2

**Table 3 Environmental correction factors (K<sub>e</sub>)**

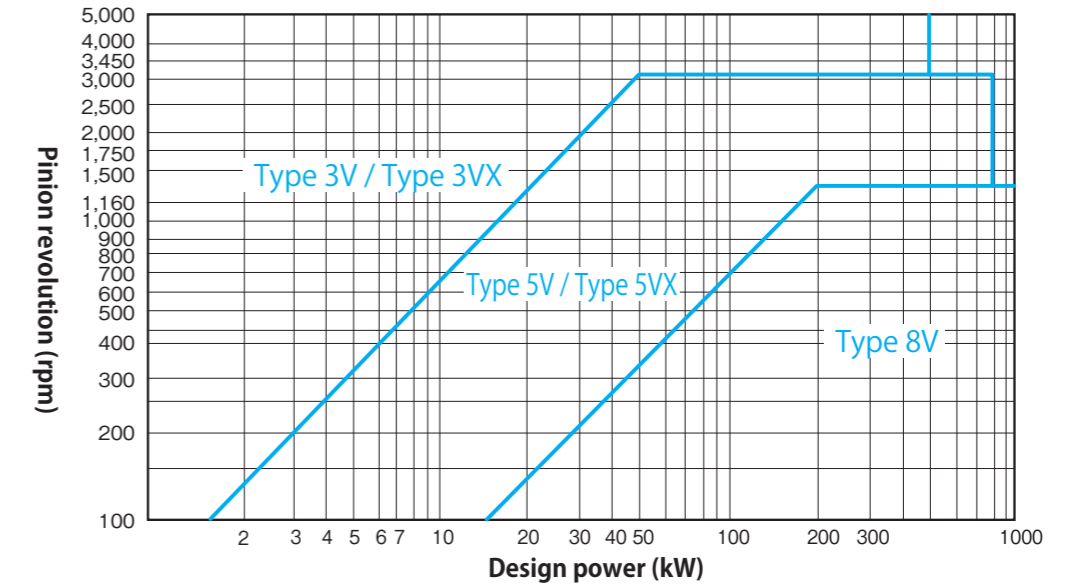
Environment	K <sub>e</sub>
Frequent starts and stops (10 times or more/day)	0.2
Difficult to maintain/inspect	0.2
Dusty and likely to abrade	0.2
High ambient temperature	0.2
Oil and water adhesion	0.2 (0.3 only in the case of Rib-Ace)

Note) For environmental correction factors, add all applicable ones.

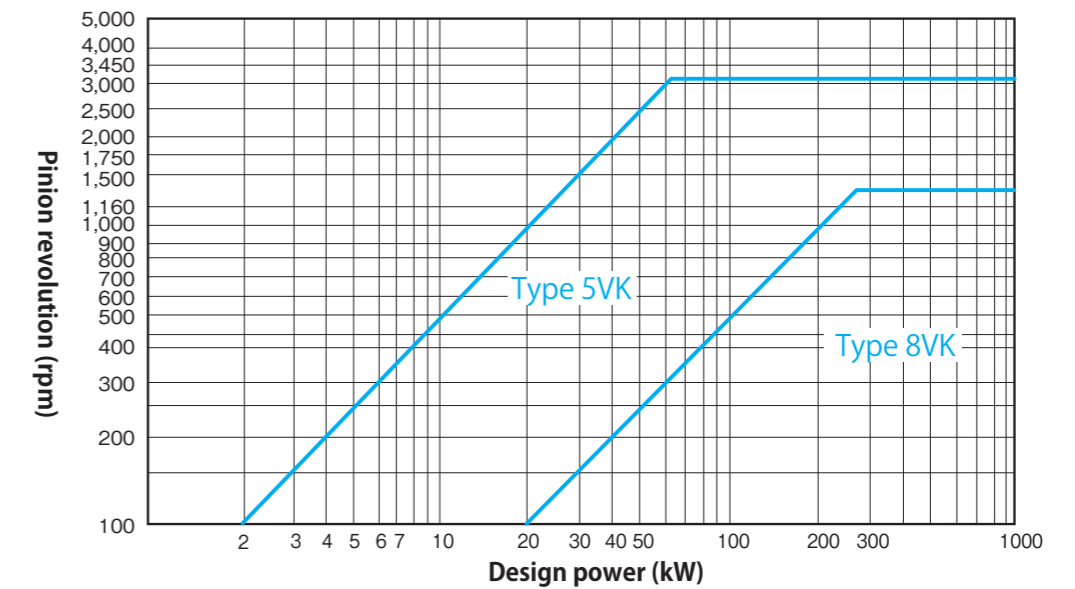
**Fig. 1-1 Belt type selection diagram (V-belts)**



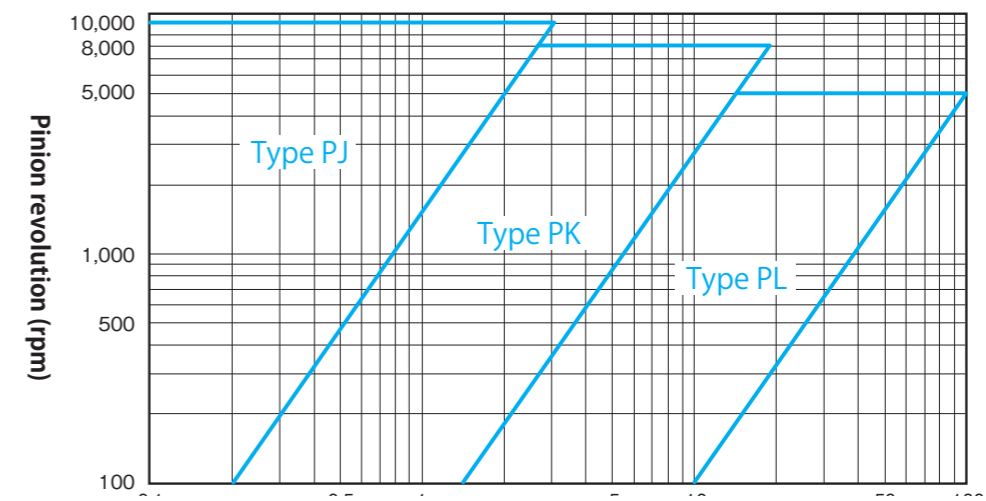
**Fig. 1-2 Belt type selection diagram (Energy-Saving Power Ace / Power Ace Cog / Power Scrum)**



**Fig. 1-3 Belt type selection diagram (Power Ace Aramid Combo)**



**Fig. 1-4 Belt type selection diagram (Rib-Ace 2)**



**Table 4 Difference between pulley outside diameter and pitch diameter (2k)**

Belt type	M	A	B	C	D	E	3V•3VX	5V•5VK•5VX	8V•8VK
2k	5.5	9.0	11.0	14.0	19.0	25.4	1.2	2.6	5.0

Pulley outside diameter = Pulley pitch diameter + 2k

**Table 5 Minimum pulley diameters**

**Table 5-1 V-belts**

Belt type	M	A	B	C	D	E
Minimum pulley pitch diameter	40	67	118	180	300	450

**Table 5-3 Rib-Ace 2**

Belt type	PJ	PK	PL
Minimum pulley outside diameter	20	50	70

**Table 6 Design belt speed standards**

Belt type	Design belt speed standard
V-belts (including Energy-Saving and Scrum types)	30 m/s or less
Power Ace (including Energy-Saving and Scrum types) / Power Ace Aramid Combo	40 m/s or less
Power Ace Cog	40 m/s or less
Rib-Ace 2	50 m/s or less

**Table of basic power ratings for Type-3V Power Ace / Power Scrum**

Pinion revolution (rpm)	Pinion nominal outside diameter (mm)																
	67	71	75	80	85	90	100	112	125	140	160	180	200	250	280	300	315
100	0.12	0.13	0.15	0.17	0.19	0.21	0.24	0.29	0.34	0.39	0.47	0.54	0.61	0.79	0.90	0.97	1.02
200	0.21	0.24	0.27	0.31	0.35	0.38	0.46	0.54	0.64	0.74	0.88	1.02	1.16	1.50	1.70	1.84	1.94
300	0.30	0.35	0.39	0.44	0.50	0.55	0.66	0.78	0.92	1.07	1.28	1.48	1.68	2.18	2.47	2.66	2.81
400	0.38	0.44	0.50	0.57	0.64	0.71	0.85	1.01	1.19	1.39	1.66	1.92	2.18	2.83	3.21	3.46	3.65
500	0.46	0.53	0.60	0.69	0.77	0.86	1.03	1.23	1.45	1.70	2.03	2.35	2.67	3.46	3.93	4.23	4.46
600	0.54	0.62	0.70	0.80	0.91	1.01	1.21	1.45	1.71	2.00	2.39	2.77	3.15	4.08	4.62	4.99	5.25
700	0.61	0.70	0.80	0.92	1.03	1.15	1.38	1.66	1.96	2.29	2.74	3.18	3.61	4.68	5.30	5.71	6.02
800	0.68	0.79	0.89	1.03	1.16	1.29	1.55	1.87	2.20	2.58	3.08	3.58	4.07	5.26	5.96	6.42	6.76
900	0.75	0.87	0.99	1.13	1.28	1.43	1.72	2.07	2.44	2.86	3.42	3.97	4.51	5.83	6.60	7.11	7.48
1000	0.81	0.94	1.08	1.24	1.40	1.56	1.89	2.27	2.68	3.14	3.75	4.36	4.95	6.39	7.23	7.77	8.17
1200	0.94	1.09	1.25	1.44	1.64	1.83	2.21	2.66	3.14	3.68	4.40	5.10	5.79	7.46	8.41	9.03	9.48
1400	1.06	1.24	1.42	1.64	1.86	2.08	2.51	3.03	3.58	4.21	5.02	5.82	6.60	8.46	9.51	10.18	10.67
1600	1.17	1.38	1.58	1.83	2.08	2.32	2.81	3.39	4.01	4.71	5.62	6.50	7.36	9.39	10.52	11.23	11.74
1800	1.28	1.51	1.73	2.01	2.29	2.56	3.10	3.74	4.42	5.19	6.19	7.16	8.09	10.25	11.43	12.15	12.67
2000	1.39	1.63	1.88	2.19	2.49	2.79	3.38	4.08	4.82	5.66	6.74	7.77	8.77	11.03	12.23	12.95	13.45
2200	1.49	1.76	2.02	2.35	2.68	3.01	3.65	4.41	5.21	6.11	7.26	8.36	9.40	11.73	12.91	13.61	14.07
2400	1.58	1.87	2.16	2.52	2.87	3.22	3.91	4.72	5.58	6.53	7.75	8.90	9.98	12.33	13.47	14.11	14.52
2600	1.67	1.98	2.29	2.68	3.05	3.43	4.16	5.03	5.93	6.94	8.21	9.41	10.51	12.84	13.90		
2800	1.76	2.09	2.42	2.83	3.23	3.63	4.41	5.32	6.27	7.32	8.64	9.87	10.98	13.24			
3000	1.84	2.19	2.54	2.97	3.40	3.82	4.64	5.59	6.59	7.68	9.04	10.29	11.40	13.53			
3200	1.92	2.29	2.66	3.11	3.56	4.00	4.86	5.86	6.89	8.02	9.41	10.66	11.75				
3400	2.00	2.39	2.77	3.25	3.71	4.17	5.07	6.11	7.18	8.33	9.74	10.98	12.04				
3600	2.07	2.47	2.88	3.37	3.86	4.34	5.27	6.34	7.44	8.62	10.04	11.25	12.25				
3800	2.13	2.56	2.98	3.49	4.00	4.50	5.46	6.57	7.69	8.88	10.29	11.47	12.40				
4000	2.19	2.64	3.07	3.61	4.13	4.65	5.64	6.77	7.91	9.12	10.51	11.63					
4500	2.33	2.81	3.29	3.87	4.43	4.98	6.04	7.22	8.39	9.57	10.86						
5000	2.44	2.96	3.46	4.08	4.68	5.26	6.36	7.56	8.71	9.83							

Pinion revolution (rpm)	Transmission capacity added depending on the speed ratio									
	1.00~1.01	1.02~1.05	1.06~1.11	1.12~1.18	1.19~1.26	1.27~1.38	1.38~1.58	1.58~1.94	1.95~3.38	3.39 or more
200	0.00	0.00	0.01	0.01	0.02	0.02	0.03	0.03	0.03	0.03
300	0.00	0.00	0.01	0.02	0.03	0.03	0.05	0.05	0.05	0.05
400	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.07	0.07
500	0.00	0.01	0.02	0.03	0.05	0.06	0.08	0.08	0.08	0.09
600	0.00	0.01	0.02	0.04	0.06	0.07	0.09	0.10	0.10	0.10
700	0.00	0.01	0.03	0.05	0.07	0.08	0.11	0.11	0.12	0.12
800	0.00	0.01	0.03	0.06	0.08	0.09	0.12	0.13	0.14	0.14
900	0.00	0.01	0.04	0.06	0.08	0.10	0.14	0.15	0.16	0.16
1000	0.00	0.01	0.04	0.07	0.09	0.11	0.15	0.16	0.17	0.17
1200	0.00	0.02	0.05	0.08	0.11	0.14	0.18	0.20	0.21	0.21
1400	0.00	0.02	0.06	0.10	0.13	0.16	0.21	0.23	0.24	0.24
1600	0.00	0.02	0.06	0.11	0.15	0.18	0.24	0.26	0.28	0.28
1800	0.00	0.03	0.07	0.12	0.17	0.21	0.27	0.29	0.31	0.31
2000	0.00	0.03	0.08	0.14	0.19	0.23	0.30	0.33	0.35	0.35
2200	0.00	0.03	0.09	0.15	0.21	0.25	0.33	0.36	0.38	0.38
2400	0.00	0.03	0.10	0.17	0.23	0.27	0.36	0.39	0.42	0.42
2600	0.00	0.04	0.10	0.18	0.25	0.30	0.39	0.42	0.45	0.45
2800	0.00	0.04	0.11	0.19	0.26	0.32	0.42	0.46	0.49	0.49
3000	0.00	0.04	0.12	0.21	0.28	0.34	0.45	0.49	0.52	0.52
3200	0.00	0.05	0.13	0.22	0.30	0.37	0.48	0.52	0.56	0.56
3400	0.00	0.05	0.14	0.24	0.32	0.39	0.51	0.55	0.59	0.59
3600	0.00	0.05	0.14	0.25	0.34	0.41	0.54	0.59	0.63	0.63
3800	0.00	0.05	0.15	0.26	0.36	0.43	0.57	0.62	0.66	0.66
4000	0.00	0.06	0.16	0.28	0.38	0.46	0.60	0.65	0.69	0.69
4500	0.00	0.06	0.18	0.31	0.42	0.51	0.68	0.73	0.78	0.78
5000	0.00	0.07	0.20	0.35	0.47	0.57	0.75	0.81	0.87	0.87

The belt speed exceeds 30 m/s. Please use pulleys made of rolled steel for general structure or carbon steel for machine construction.

























# How to Design a Frictional Transmission Belt

## Power Ace Design Example

### Step 1. Determining conditions required for the design

- Driving machine: Induction motor 45 kW/1160 rpm
- Driven machine: Piston pump (24-hour/day continuous operation)
- Driven pulley 600 rpm/ $\phi$  520 mm (do)
- Center distance 1150mm
- Minimum maintenance and inspection

### Step 2. Calculating the design power

- Obtain the load correction factor from **Table 1** ( $\rightarrow$  P. 247).  
 $K_o=1.4$
- Obtain the idler correction factor and the environmental correction factor from **Table 2** and **Table 3** ( $\rightarrow$  P. 247).  
 $K_i=0.0$   $K_e=0.2$
- Therefore, the design power is 72 kW.  
 $P_d=45 \times (1.4+0.0+0.2) = 72\text{kW}$

### Step 3. Selecting a belt type

From the design power of 72 kW and the pinion revolution of 1160 rpm from **Fig. 1 Belt type selection diagram** ( $\rightarrow$  P. 248), select Type 5V.

### Step 4. Selecting a pulley diameter

- The speed ratio is  $1160 / 600 = 1.93$
- Assuming the large-pulley nominal outside diameter is 520 mm, from the speed ratio calculation, set the pinion nominal outside diameter to 270 mm.  
$$\frac{520 - 2.6}{1.93} + 2.6 \approx 270 \text{ mm}$$
- Satisfy the minimum nominal outside diameter of a pulley of 150 mm for Type 5V.
- The belt speed satisfies 40 m/s or less.  
$$\frac{(270-2.6) \times 1160}{19100} = 16.2\text{m/s}$$

### Step 5. Selecting an effective length

- The effective length calculation results in 3554 mm, and from the **list of belt sizes** ( $\rightarrow$  P. 230), select 5V1400(effective outside length 3556 mm).  
$$2 \times 1150 + 1.57(520+270) + \frac{(520-270)^2}{4 \times 1150} = 3554\text{mm}$$
- From the effective outside length of the selected belt, the center distance is 1151 mm.  
$$B=3556-1.57(520+270)=2316$$
  
$$C = \frac{2316 + \sqrt{2316^2 - 2(520 - 270)^2}}{4}$$
  
$$= 1151\text{mm}$$

### Step 6. Determining the number of belts

- In the **Table of basic power ratings for 5V** ( $\rightarrow$  P. 251), obtain the transmission capacity for the pinion revolution of 1160 rpm and the pinion nominal outside diameter of 270 mm by proportional distribution as shown below, and add an additional capacity by the speed ratio to obtain the transmission capacity.

Pinion revolution (rpm)	Pinion nominal diameter (mm)		Transmission capacity added depending on the speed ratio (kW/pc)
	260	280	
1160	17.34	19.16	1.58 }
			1.94
			0.99

- Obtain the effective length correction factor  $K_l$  from **Table 7** ( $\rightarrow$  P. 271).  
 $K_l = 1.02$
- Obtain the contact angle correction factor  $K_{\theta_1}$  from **Table 8** ( $\rightarrow$  P. 272).  
 $K_{\theta_1} = 0.97$
- Therefore, the number of belts is 4.  
$$N = \frac{72}{19.24 \times 0.97 \times 1.02} = 3.8 \rightarrow 4 \text{ belts}$$

### Step 7. Checking the adjustment range of the center distance

From **Table 9** ( $\rightarrow$  P. 272), obtain  $C_i$  and  $C_s$ .  
 $C_i=25\text{mm}$   
 $C_s=56\text{mm}$

### Examination result

- Belt 5V1400  $\times$  4
- Pinion (driving pulley) nominal outside diameter: 270 mm
- Large (driven) pulley nominal outside diameter: 520 mm
- Center distance 1151 mm
  - Inner minimum adjustment range: 25 mm
  - Outer minimum adjustment range: 56 mm

Design power: 72 kW

Belt type: 5 V

Large-pulley nominal outside diameter: 520 mm  
Pinion nominal outside diameter: 270 mm

Effective length: 5V1400

Center distance: 1151mm

Basic power rating = 19.24 kW/pc

$K_l = 1.02$

$K_{\theta_1} = 0.97$

Number of belts = 4 belts

Inner minimum adjustment range ( $C_i$ ) = 25 mm  
Outer maximum adjustment range ( $C_s$ ) = 56 mm